

## **APÉNDICES**

## APÉNDICE I

### Resultados obtenidos del sistema de 13 barras bajo la metodología NIHA

A continuación se presentan los resultados de la penetración armónica bajo la metodología NIHA en Matpower:

MATPOWER Version 5.1, 20-Mar-2015 -- AC Harmonic Power Flow Calculation				
MATPOWER Version 5.1, 20-Mar-2015 -- AC Power Flow (Newton)				
Newton's method power flow converged in 3 iterations.				
Converged in 0.08 seconds				
=====				
System Summary				
=====				
=====				
How many?	How much?	P (MW)	Q (MVar)	
-----				
Buses	13	Total Gen Capacity	200.0	0.0 to 100.0
Generators	2	On-line Capacity	200.0	0.0 to 100.0
Committed Gens	2	Generation (actual)	9.4	2.4
Loads	7	Load	9.3	7.6
Fixed	7	Fixed	9.3	7.6
Dispatchable	0	Dispatchable	-0.0 of -0.0	-0.0
Shunts	1	Shunt (inj)	-0.0	5.9
Branches	12	Losses (I <sup>2</sup> * Z)	0.08	0.75
Transformers	7	Branch Charging (inj)	-	0.0
Inter-ties	0	Total Inter-tie Flow	0.0	0.0
Areas	1			
-----				
		Minimum	Maximum	
-----				
Voltage Magnitude		0.979 p.u. @ bus 12	1.006 p.u. @ bus 13	
Voltage Angle		-4.58 deg @ bus 8	0.00 deg @ bus 1	
P Losses (I <sup>2</sup> *R)		-	0.02 MW @ line 4-5	
Q Losses (I <sup>2</sup> *X)		-	0.29 MVar @ line 4-5	

Bus Data						
Bus #	Voltage		Generation		Load	
	Mag(pu)	Ang(deg)	P (MW)	Q (MVAr)	P (MW)	Q (MVAr)
1	1.000	0.000*	7.36	0.54	-	-
2	0.995	-2.359	2.00	1.86	-	-
3	0.996	-3.446	-	-	0.60	0.53
4	0.999	-0.121	-	-	-	-
5	0.995	-2.370	-	-	2.24	2.00
6	0.994	-2.372	-	-	-	-
7	1.002	-4.566	-	-	1.15	0.29
8	1.001	-4.578	-	-	1.31	1.13
9	0.994	-2.368	-	-	-	-
10	0.984	-3.855	-	-	0.81	0.80
11	0.994	-2.367	-	-	-	-
12	0.979	-3.048	-	-	0.37	0.33
13	1.006	-4.430	-	-	2.80	2.50
Total:			9.36	2.40	9.28	7.58

  

Branch Data								
Brnch #	From Bus	To Bus	From Bus P (MW)	Injection Q (MVAr)	To Bus P (MW)	Injection Q (MVAr)	Loss P (MW)	Loss Q (MVAr)
1	1	4	7.36	0.54	-7.35	-0.52	0.008	0.02
2	2	3	0.60	0.55	-0.60	-0.53	0.004	0.02
3	2	5	1.40	1.31	-1.40	-1.30	0.000	0.00
4	4	5	7.35	0.52	-7.33	-0.23	0.017	0.29
5	5	6	2.48	1.57	-2.48	-1.57	0.001	0.00
6	5	9	0.82	0.85	-0.82	-0.85	0.000	0.00
7	5	11	3.19	3.04	-3.19	-3.04	0.002	0.00
8	6	7	1.16	0.34	-1.15	-0.29	0.008	0.05
9	6	8	1.32	1.23	-1.31	-1.13	0.013	0.10
10	9	10	0.82	0.85	-0.81	-0.80	0.008	0.05
11	11	12	0.37	0.34	-0.37	-0.33	0.001	0.01
12	11	13	2.82	2.70	-2.80	-2.50	0.017	0.20
Total:							0.080	0.75

System Summary					
How many?					
Buses	13				
Generators	2				
Committed Gens	2				
Loads	7				
Fixed	6				
Dispatchable	0				
Total NON_LOAD	1				
Shunts	1				
Branches	12				
Transformers	7				
Areas	1				
Number bus NON_LOAD	7				
harmonic (spectrum)	37				
Maximum					
Bus Data					
bus	V1(L-N)	V3(L-N)	V5(L-N)	V7(L-N)	THDv[%]
1	39837.2	0	42.5964	103.715	0.283155
2	7927.6	0	55.0037	133.912	1.83718
3	276.124	0	1.90449	4.60956	1.81673
4	39790.2	0	55.3526	134.75	0.368328
5	7923.69	0	56.8853	138.501	1.90107
6	7921.41	0	57.4411	138.624	1.90499
7	277.654	0	12.6249	11.6929	7.46203
8	2404.6	0	17.0598	40.3175	1.82954
9	7921.77	0	56.8673	138.448	1.90081
10	272.642	0	1.93559	4.66144	1.86163
11	7918.69	0	56.8361	138.351	1.90026
12	271.446	0	1.94388	4.72113	1.8921
13	1393.67	0	9.82627	23.511	1.83821

## APÉNDICE II

### Archivo caso13barras.m

A continuación se presenta la estructura “mpc” que almacena los datos del sistema de trece (13) barras para la solución de penetración armónica bajo la metodología IHA en Matpower:

```
function mpc = caso13barras
% Harmonic Power flow data A 13-Bus Balanced Industrial Distribution System
% MATPOWER
% Id: caso13barras.m
%% MATPOWER Case Format : Version 2
mpc.version = '2';

%%----- Power Flow Data -----%%
%% system MVA base
mpc.baseMVA = 10;

%% bus data
% bus_i type Pd Qd Gs Bs area Vm Va baseKV zone Vmax Vmin nonl_load
mpc.bus = [
    1 3 0 0 0 0 1 1 0 69 1 1.05 0.95 0;
    2 2 0 0 0 0 1 1 0 13.8 2 1.05 0.95 0;
    3 1 0.6 0.53 0 0 1 1 0 0.48 4 1.05 0.95 0;
    4 1 0 0 0 0 1 1 0 69 1 1.05 0.95 0;
    5 1 2.24 2 0 6 1 1 0 13.8 3 1.05 0.95 0;
    6 1 0 0 0 0 1 1 0 13.8 3 1.05 0.95 0;
    7 1 0.049 0.082 0 0 1 1 0 0.40 5 1.05 0.95 1;
    8 1 1.31 1.13 0 0 1 1 0 4.16 6 1.05 0.95 0;
    9 1 0 0 0 0 1 1 0 13.8 3 1.05 0.95 0;
    10 1 0.81 0.8 0 0 1 1 0 0.48 7 1.05 0.95 0;
    11 1 0 0 0 0 1 1 0 13.8 3 1.05 0.95 0;
    12 1 0.37 0.33 0 0 1 1 0 0.48 8 1.05 0.95 0;
    13 1 2.8 2.5 0 0 1 1 0 2.4 9 1.05 0.95 0;
];

%% generator data
% bus Pg Qg Qmax Qmin Vg mBase status Pmax Pmin Pc1 Pc2 Qc1min Qc1max Qc2min
% Qc2max ramp_agc ramp_10 ramp_30 ramp_q apf Rg Xg
mpc.gen = [
    1 0 0 50 0 1 10 1 100 0 0 0 0 0 0
0 0 0 0 0 0 0 0 0.00045 0.00990;
    2 2 0 50 0 0.995 10 1 100 0 0 0 0 0 0
0 0 0 0 0 0 0 0 0.00192 0.07168;
];
```

```

%% branch data
% fbus tbus r x b rateA rateB rateC ratio angle status angmin angmax
mpc.branch = [
  1 4 0.00139 0.00296 0 150 0 0 0 0 1 -360 360;
  2 3 0.06391 0.37797 0 150 0 0 0.975 0 1 -360 360;
  2 5 0.00122 0.00243 0 150 0 0 0 0 1 -360 360;
  4 5 0.00313 0.05324 0 150 0 0 1 0 1 -360 360;
  5 6 0.00075 0.00063 0 150 0 0 0 0 1 -360 360;
  5 9 0.00157 0.00131 0 150 0 0 0 0 1 -360 360;
  5 11 0.00109 0.00091 0 150 0 0 0 0 1 -360 360;
  6 7 0.05918 0.35510 0 150 0 0 0.975 0 1 -360 360;
  6 8 0.04314 0.34514 0 150 0 0 0.95 0 1 -360 360;
  9 10 0.05829 0.37888 0 150 0 0 0.975 0 1 -360 360;
  11 12 0.05575 0.36240 0 150 0 0 1 0 1 -360 360;
  11 13 0.01218 0.14616 0 150 0 0 0.95 0 1 -360 360;
];

```

## APÉNDICE III

### Función `runpfH2.m`

A continuación se presenta el código en Matpower para la función `runpfH2`:

```
function [MVAbase, bus, gen, branch, success, et] = runpfH2(casedata, mpopt)

%%----- initialize -----

close all; clear all; clc;
% iacm: corriente medida
% vacm: voltaje medido
% PhVk, PhIk : fasores de voltaje y corriente (numeros complejos) medidos
Nh=100; %armonicos de voltaje
NLamp=1000; %numero de lamparas

%% Declaraciones de constantes generales
fs=60;ws=2*pi*fs; % frecuencia
Ts=1/fs; % Periodo del fundamental
Ns=10000; % número de muestras
ts = linspace(0,Ts,Ns); % rango de simulación en el tiempo
Hmax=2*Nh-1; % número de armónicos y armónico máximo
Nmax=Hmax;
k1=(1:2:Hmax)'; % vector columna de armónicos

%% Definición de los nombres de los índices de las matrices bus, gen, branch
% 1 2 3 4 5 6 7 8 9 10 11 12 13 14
[PQ, PV, REF, NONE, BUS_I, BUS_TYPE, PD, QD, GS, BS, BUS_AREA, VM, VA, BASE_KV,...
ZONE, VMAX, VMIN, NONL_LOAD, LAM_P, LAM_Q, MU_VMAX, MU_VMIN] = idx_busH;
% 15 16 17 18 19 20 21 22

[F_BUS, T_BUS, BR_R, BR_X, BR_B, RATE_A, RATE_B, RATE_C, ...
TAP, SHIFT, BR_STATUS, PF, QF, PT, QT, MU_SF, MU_ST, ...
ANGMIN, ANGMAX, MU_ANGMIN, MU_ANGMAX] = idx_brchH ;

[GEN_BUS, PG, QG, QMAX, QMIN, VG, MBASE, GEN_STATUS, PMAX, PMIN, ...
MU_PMAX, MU_PMIN, MU_QMAX, MU_QMIN, PC1, PC2, QC1MIN, QC1MAX, ...
QC2MIN, QC2MAX, RAMP_AGC, RAMP_10, RAMP_30, RAMP_Q, APF, RG, XG] = idx_genH;

%% Definición de argumentos
if nargin < 4
    solvedcase = " ; %% don't save solved case
if nargin < 3
    fname = " ; %% don't print results to a file
if nargin < 2
    mpopt = mpoption; %% use default options
if nargin < 1
```

```

        casedata = 'caso13barras'; %% default data file is 'case13paper.m'
    end
    end
    end
end

%% Leer datos
mpc = loadcase(casedata);

%% Conversion interna
mpc = ext2int(mpc);
[baseMVA, bus, gen, branch] = deal(mpc.baseMVA, mpc.bus, mpc.gen, mpc.branch);

%% Correr flujo de carga convencional
t0 = clock;
if mpc.verbose > 0
    v = mpver('all');
    fprintf('\nMATPOWER Version %s, %s', v.Version, v.Date);
end

%% Formulación
fprintf(' -- AC Harmonic Power Flow Calculation \n');
[MVAbase, bus, gen, branch, success, et] = runpf(casedata);

if mpc.verbose
    fprintf('\nHarmonics Power Flow through iterative harmonic analysis method (IHA)\n');
end

success = 1;
mpc.et = etime(clock, t0);
mpc.success = success;
et=mpc.et;
fd=1;

%% Fasor de voltajes fundamentales de barras
Vbusf=bus(:,VM);
PHVbusf=bus(:,VA)*pi/180;
PhVbusf=Vbusf.*exp(1j*PHVbusf);

%% Extraer datos de voltaje en barra con carga CFL
nonL=find(bus(:,NONL_LOAD)); % Se toma los números de las barras en donde están las cargas no
lineales
V1=bus(nonL,VM);
PHV1=bus(nonL,VA)*pi/180; % ángulo en radianes

%% voltaje inicial, solo fundamental en por unidad
PhVh=[V1*exp(1j*PHV1);zeros(Nh-1,1)];
Vh=abs(PhVh);
THDv1=norm(Vh(2:end))*100;

%% Primera iteración
[PhIh, ykk] =Currents_Phase_CFL(PhVh,MVAbase,bus(nonL,BASE_KV),NLamp);
Ih=abs(PhIh);PHIh=angle(PhIh); % modulo y fase corriente simulada

```

```

%% Corriente inicial en función del tiempo de la corriente simulada
iacn=zeros(Ns,1);
for i=1:Ns
    iacn(i)=sqrt(2)*sum(Ih.*cos(k1.*ws*ts(i)+PHIh));
end

%% cantidades bases
Ibase_sys=1e3*MVAbase/(sqrt(3)*bus(nonL,BASE_KV));
Irms=norm(Ih)*Ibase_sys;

Vbase_nonL=bus(nonL,BASE_KV)*1e3;
Vrms1=norm(Vh)*Vbase_nonL;

%% lazo iterativo para determinar las tensiones armónicas de las barras
%% Tamaño de cosas
nb = size(bus, 1);    %% Numero de barras
nl = size(branch, 1); %% Numero de ramas
ng = size(gen, 1);   %% Numero de generadores

E=1;
Vhar=zeros(nb,Nh);
Vharo(:,1)=PhVbusf;

while E>0.005

    for j=1:Nh; % vector de armónicos
        k=2*j-1;

        YbusH=makeYbusH_v3(baseMVA,bus,branch,gen,k) + ...
            sparse(nonL,nonL,ykk(j),nb,nb); % Matriz de admitancia armónica
        Ihar= -bus(:,NONL_LOAD).*PhIh(j); % vector de corrientes de barra
        Vhar(:,j)=YbusH\Ihar; % matriz de tensiones de barra
    end
    Vhar(:,1)=Vharo(:,1)+Vhar(:,1);

    THDv=sqrt(sum(abs(Vhar(nonL,2:end)).^2,2))./abs(Vhar(nonL,1))*100;
    E=abs(THDv-THDv1);
    [PhIh, ykk] =Currents_Phase_CFL(Vhar(nonL,:)',MVAbase,bus(nonL,BASE_KV),NLamp);

    THDv1=THDv;
    Vharo(:,1)=Vhar(:,1);
end

%% Corriente considerando el voltaje distorsionado
Ih1=abs(PhIh);PHIh1=angle(PhIh); % modulo y fase de la corriente simulada con distorsión
Irms1=norm(Ih1)*Ibase_sys;

%% corriente final en función del tiempo de la corriente simulada
iacn=zeros(Ns,1);
for i=1:Ns
    iacn(i)=sqrt(2)*sum(Ih1.*cos(k1.*ws*ts(i)+PHIh1));
end

```

```

%% Tensión en función del tiempo
Vf=Vh;PHVf=angle(Vh); % modulo y fase de la tensión fundamental en la barra de carga no lineal
Vh7=abs(Vhar(nonL,:)); PHVh7=angle(Vhar(nonL,:)); % modulo y fase de la tensión distorsionada
en la barra de carga no lineal
Vbase_nonL=bus(nonL,BASE_KV)*1e3; %tensión base en la barra de carga no lineal
Vrms=norm(Vh7)*Vbase_nonL; % voltaje trifásico en kV

SnonL=sqrt(3)*Vrms*Irms1/1e3 % potencia aparente trifásica kVA
PnonL=sum(Vh7.*Ih1.*cos(PHVh7-PHIh1))*MVAbase*1e3 %potencia activa en kW
fp_nonL=PnonL/SnonL %factor de potencia
QnonL=sqrt(SnonL*SnonL-PnonL*PnonL) %potencia reactiva en kVar

vacn=zeros(Ns,1);
vacn1=zeros(Ns,1);
for i=1:Ns
    vacn1(i)=sqrt(2)*sum(Vf.*cos(k1.*ws*ts(i)+PHVf));
    vacn(i)=sqrt(2)*sum(Vh7.*cos(k1.*ws*ts(i)+PHVh7));
end

%% Gráficas
figure(1)
plot(ts*1e3,iacn*Ibase_sys,'b',ts*1e3,iacn1*Ibase_sys,'r')
legend('I_f_u_n_d','I_h_a_r_m',2);
title(['I_rms_f_u_n_d = ',num2str(Irms), 'A', ' I_rms_h_a_r_m = ',num2str(Irms1), 'A'])
ylabel('Corriente (A)')
xlabel('Tiempo (ms)')
grid on

fk=Vbase_nonL/sqrt(3); % voltaje monofásico

figure(2)
plot(ts*1e3,vacn1*fk,'b',ts*1e3,vacn*fk,'r');
legend('V_f_u_n_d','V_h_a_r_m',4);
title(['V_rms_f_u_n_d = ',num2str(Vrms1/sqrt(3)), 'V', ' V_rms_h_a_r_m = ',num2str(Vrms/sqrt(3)), 'V'])
ylabel('Tensión (V)')
xlabel('Tiempo (ms)')
grid on

%% Diagrama de tiempo y barras combinados
figure(40)
subplot(2,1,1)
plot(ts*1e3,iacn*Ibase_sys,'b');hold on
plot(ts*1e3,iacn1*Ibase_sys,'r');
legend('I_f_u_n_d','I_h_a_r_m',4);
title(['P_c_f_1 = ',num2str(PnonL), 'kW', ' S_c_f_1 = ',num2str(SnonL), 'kVA', ' fp_c_f_1 = ',num2str(fp_nonL)])
ylabel('Corriente (A)')
xlabel('Tiempo (ms)')
grid on
subplot(2,1,2)
bar(k1,[Ih,Ih1]*Ibase_sys)
title(['I_rms_f_u_n_d = ',num2str(Irms), 'A', ' I_rms_h_a_r_m = ',num2str(Irms1), 'A'])
legend('I_f_u_n_d','I_h_a_r_m',1);

```

```

xlabel('Armónico (h)')
ylabel('Amplitud (A)')
xlim([0 14])
ylim([0 110])
grid on

figure (50)
subplot(2,1,1)
plot(ts*1e3,vacn1*fk,'b',ts*1e3,vacn*fk,'r');
legend('V_f_u_n_d','V_h_a_r_m',4);
title(['Vrms_f_u_n_d = ',num2str(Vrms1/sqrt(3)), 'V,' Vrms_h_a_r_m = ',num2str(Vrms/sqrt(3)), 'V'])
ylabel("Tensión (V)")
xlabel("Tiempo (ms)")
grid on
subplot(2,1,2)
bar(k1,[Vf,Vh7]*fk)
title(['THD_v = ',num2str(THDv), '%'])
legend('V_f_u_n_d','V_h_a_r_m',1);
xlabel('Armónico (h)')
ylabel('Amplitud (V)')
xlim([2 51])
grid on

%% Importación del Fourier de corriente del "Pspice
%%para la lámpara 2
filename = 'FourIlamp2.txt';
delimiterIn = ' ';
headerlinesIn = 4;
A = importdata(filename,delimiterIn,headerlinesIn);
MIpsp=A.data(1:2:end,3)/sqrt(2); % Valor rms de las amplitudes de corriente, armónicos impares

Irms2=norm(MIpsp);

r1=(1:2:15);% rango armónico
figure(60)
bar(r1,[Ih1(1:8,1)*Ibase_sys,MIpsp])
title(['Irms_h_a_r_m = ',num2str(Irms1), 'A,' Irms_P_s_p_i_c_e = ',num2str(Irms2), 'A'])
legend('I_c_f_l_h_a_r_m','I_c_f_l_P_s_p_i_c_e',1);
xlabel('Armónico (h)')
ylabel('Amplitud (A)')
xlim([0 16])
ylim([0 110])
grid on

%% Importación de la onda de corriente del "Pspice
%%para la lampara 2
filename = 'TimeIlamp2.txt';
%filename = 'Timellamp1.txt';
delimiterIn = ' ';
headerlinesIn = 13;
A = importdata(filename,delimiterIn,headerlinesIn);
ipsp=A.data(:,4);
t1=linspace(0,20/1000,10000);

```

```

figure(70)
plot(ts*1e3,iacn1*ibase_sys,'r');hold on
plot(t1*1e3,ipsp);
title(['Irms_h_a_r_m = ',num2str(Irms1), 'A,' Irms_P_s_p_i_c_e = ',num2str(Irms2), 'A'])
legend('I_c_f_l_-_h_a_r_m','I_c_f_l_-_P_s_p_i_c_e',2)
ylabel('Corriente (A)')
xlabel('Tiempo (ms)')
grid on

%% Determinación de la tasa de distorsión de armónico THD
idx_paper=[1,4,5,2,3,6,7,8,9,11,12,13,10];
abs(Vhar(idx_paper,1)).*bus(idx_paper,BASE_KV)/sqrt(3)*1000; % fundamental
abs(Vhar(idx_paper,3)).*bus(idx_paper,BASE_KV)/sqrt(3)*1000; % 5 armonico
abs(Vhar(idx_paper,4)).*bus(idx_paper,BASE_KV)/sqrt(3)*1000; % 7 armonico
THDv = sqrt(sum(abs(Vhar(:,2:end)).^2,2))./abs(Vhar(:,1))*100; % Tasa distorsion
THDv(idx_paper);
%% creación de un vector externo de los índices de las barras
i2e = bus(:, BUS_I) ;

% Parámetros
g1=find(bus(:,NONL_LOAD));
%
OUT_ALL      = mpopt.out.all;
OUT_FORCE    = mpopt.out.force;
SUPPRESS     = mpopt.out.suppress_detail;
%
if SUPPRESS == -1
    if size(bus, 1) > 500
        SUPPRESS = 1;
    else
        SUPPRESS = 0;
    end
end
OUT_SYS_SUM  = OUT_ALL == 1 || (OUT_ALL == -1 && mpopt.out.sys_sum);
OUT_BUS      = OUT_ALL == 1 || (OUT_ALL == -1 && ~SUPPRESS && mpopt.out.bus);
% áreas
xfmr = find(branch(:, TAP));          %% indices of transformers
nzld = find((bus(:, PD) | bus(:, QD)) & bus(:, BUS_TYPE) ~= NONE); % barras donde hay cargas
lineales
sorted_areas = sort(bus(:, BUS_AREA)); % áreas del sistema
s_areas = sorted_areas([1; find(diff(sorted_areas))+1]); %% números de áreas
nzsh = find((bus(:, GS) | bus(:, BS)) & bus(:, BUS_TYPE) ~= NONE); % barras donde hay
elementos shunt
allg = find( ~isload(gen) ); % barras donde hay generación
ong  = find( gen(:, GEN_STATUS) > 0 & ~isload(gen) );
onld = find( gen(:, GEN_STATUS) > 0 & isload(gen) );
%% Resumen del sistema
if OUT_SYS_SUM && (success || OUT_FORCE)
    fprintf(fd,
\n=====
=====');
    fprintf(fd, \n|   System Summary                               |);

```

```

fprintf(fd,
\n=====
=====');
fprintf(fd, \n\n          How many?          ');
fprintf(fd, \n-----');
fprintf(fd, \nBuses          %6d          ', nb);
fprintf(fd, \nGenerators          %6d          ', length(allg));
fprintf(fd, \nCommitted Gens          %5d          ', length(ong));
fprintf(fd, \nLoads          %5d          ', length(nzld)+length(onld));
fprintf(fd, \n Fixed          %5d          ', length(nzld)-sum(bus(:,NONL_LOAD)));
fprintf(fd, \n Dispatchable          %5d          ', length(onld));
fprintf(fd, \n Total NON_LOAD          %5d          ',sum(bus(:,NONL_LOAD)));
fprintf(fd, \nShunts          %5d          ', length(nzsh) );
fprintf(fd, \nBranches          %5d          ', nl );
fprintf(fd, \nTransformers          %5d          ', length(xfmr) );
fprintf(fd, \nAreas          %5d', length(s_areas));
fprintf(fd, \nNumber bus NON_LOAD          %5d          ', g1);
fprintf(fd, \nMaximum');
fprintf(fd, \n-----');
Vharm=zeros(nb,4);
for j=1:nb
    Vharm(j,1:4)=abs(Vhar(j,1:4))*bus(j,BASE_KV)/sqrt(3)*1000;
end
end
%% data de la barras- Tensiones armónicas
if OUT_BUS && (success || OUT_FORCE)
    fprintf(fd,
\n=====
=====
=====
=====
=====');
    fprintf(fd, \n|          Bus Data
|');
    fprintf(fd,
\n=====
=====
=====
=====
=====');
    fprintf(' bus ')
    for k=1:2:7
        fprintf(fd, ' V%d(L-N) \t',k);
    end
    fprintf(fd, ' THDv[%%]\n')
    for j=1:nb
        fprintf(fd, ' %g\t',bus(j, BUS_I));
        fprintf(fd, ' %g \t',Vharm(j,1:4));
        fprintf(fd, ' %g \t',THDv(j));
        fprintf(fd, ' \n');
    end
end
end
end

```

## APÉNDICE IV

### Función Currents\_Phazor\_CFL.m

A continuación se presenta el código en Matpower para la función Currents\_Phazor\_CFL:

```
function [PhIh,ykk]=Currents_Phazor_CFL(PhVh,MVA_base,KV_base,NLamp)
% PhVh = fasor de voltajes armónicos = Vh*exp(j*PHVh) en pu
% Vh = amplitud del fasor PhVh = abs(PhHh)
% PHVh = fase del fasor PhVh
% Nk = número total de armónicos
% ws = frecuencia electrica
Nk=size(PhVh,1); % número de armónicos de tensión
Nh=Nk; % armónicos de corriente
fs=60; ws=2*pi*fs;
Kmax=2*Nk-1; % número de armónicos y armónico máximo
%Hmax=Kmax;
Hmax=2*Nh-1;

%% -----Lámpara a simular-----
Lamp=1;Type=3;archivo=1;
[RD,R,C]=ficheroDatosCFL(Lamp,Type,archivo);
rN=R/RD; XcN=1e6/(ws*C*RD);Xc=1e6/(ws*C);
%% -----
Nroh=7;
PhVh=[PhVh(1:Nroh);zeros(Nh-Nroh,1)]; % solo se consideran hasta el armónico 13 de voltaje
%% Voltaje y corriente rms, medidos-----
VhN=PhVh; % Voltajes normalizado pu
%% Taza de distorsión armónica de voltaje-----
THDv = norm(VhN(2:end))*100;
%% Ángulos de conmutación-----
PHi=[-0.20 2.0]; % Valor inicial
PH=Funcion_PH(XcN,rN,VhN,Nk,PHi); % ángulo de conmutación simulados

%% Modelo de matrices Y-----
if THDv <= 1
    [Yh,Ykk]=FunMatrixYA4(VhN,R,Xc,RD,PH,Kmax,Hmax);
elseif THDv >1 && THDv <= 4
    [Yh,Ykk]=FunMatrixYA3(VhN,R,Xc,RD,PH,Kmax,Hmax);
elseif THDv >4 && THDv <= 6
    [Yh,Ykk]=FunMatrixYA2(VhN,R,Xc,RD,PH,Kmax,Hmax);
elseif THDv >6 && THDv <= 8
    [Yh,Ykk]=FunMatrixYA1(VhN,R,Xc,RD,PH,Kmax,Hmax);
else
    [Yh,Ykk]=FunMatrixYF(VhN,R,Xc,RD,PH,Kmax,Hmax);
End
```

```

%% Valores base del sistema -----
Ibase_sys=1e3*MVA_base/(sqrt(3)*KV_base);
Zbase_sys=(1e3*KV_base/sqrt(3))/Ibase_sys;
%% Valores base del cfl -----
Ibase_cfl=(1e3*KV_base/sqrt(3))/RD;
Zbase_cfl=RD;
%% Corriente armónica
Phlh=NLamp*Yh*PhVh; %corriente en pu
Phlh=Phlh*Ibase_cfl/Ibase_sys; % valor en pu base sys
%% admintacia propis
ykk=diag(Ykk);
ykk=ykk*1/Zbase_cfl; %admitancia en siemens
ykk=ykk/(1/Zbase_sys); % admitancia en pu base sys
ykk=NLamp*ykk;
end

```

## APÉNDICE V

### Resultados obtenidos del sistema de 13 barras bajo la metodología IHA

A continuación se presentan los resultados de la penetración armónica bajo la metodología IHA en Matpower:

#### - Caso 1: CFL – L1P11W

MATPOWER Version 5.1, 20-Mar-2015 -- AC Harmonic Power Flow Calculation				
MATPOWER Version 5.1, 20-Mar-2015 -- AC Power Flow (Newton)				
Newton's method power flow converged in 3 iterations.				
Converged in 0.04 seconds				
=====				
System Summary				
=====				
How many?	How much?	P (MW)	Q (MVAr)	
-----				
Buses	13	Total Gen Capacity	200.0	0.0 to 100.0
Generators	2	On-line Capacity	200.0	0.0 to 100.0
Committed Gens	2	Generation (actual)	8.2	2.0
Loads	7	Load	8.2	7.4
Fixed	7	Fixed	8.2	7.4
Dispatchable	0	Dispatchable	-0.0 of -0.0	-0.0
Shunts	1	Shunt (inj)	-0.0	5.9
Branches	12	Losses (I <sup>2</sup> * Z)	0.06	0.61
Transformers	7	Branch Charging (inj)	-	0.0
Inter-ties	0	Total Inter-tie Flow	0.0	0.0
Areas	1			
		Minimum	Maximum	
		-----		
Voltage Magnitude	0.980 p.u. @ bus 12	1.017 p.u. @ bus 7		
Voltage Angle	-4.21 deg @ bus 8	0.00 deg @ bus 1		
P Losses (I <sup>2</sup> *R)	-	0.02 MW @ line 11-13		
Q Losses (I <sup>2</sup> *X)	-	0.21 MVAr @ line 4-5		

Bus Data						
Bus #	Voltage		Generation		Load	
	Mag(pu)	Ang(deg)	P (MW)	Q (MVar)	P (MW)	Q (MVar)
1	1.000	0.000*	6.24	0.57	-	-
2	0.995	-1.994	2.00	1.47	-	-
3	0.996	-3.081	-	-	0.60	0.53
4	0.999	-0.101	-	-	-	-
5	0.995	-2.007	-	-	2.24	2.00
6	0.994	-2.006	-	-	-	-
7	1.017	-2.082	-	-	0.05	0.07
8	1.001	-4.212	-	-	1.31	1.13
9	0.994	-2.005	-	-	-	-
10	0.984	-3.492	-	-	0.81	0.80
11	0.994	-2.685	-	-	-	-
12	0.980	-2.685	-	-	0.37	0.33
13	1.006	-4.067	-	-	2.80	2.50
Total:			8.24	2.04	8.18	7.36

  

Branch Data								
Brnch #	From Bus	To Bus	From Bus P (MW)	From Bus Q (MVar)	To Bus P (MW)	To Bus Q (MVar)	Loss (I <sup>2</sup> * Z)	
			P (MW)	Q (MVar)	P (MW)	Q (MVar)	P (MW)	Q (MVar)
1	1	4	6.24	0.57	-6.24	-0.55	0.005	0.01
2	2	3	0.60	0.55	-0.60	-0.53	0.004	0.02
3	2	5	1.40	0.91	-1.40	-0.91	0.000	0.00
4	4	5	6.24	0.55	-6.23	-0.35	0.012	0.21
5	5	6	1.37	1.30	-1.37	-1.30	0.000	0.00
6	5	9	0.82	0.85	-0.82	-0.85	0.000	0.00
7	5	11	3.19	3.04	-3.19	-3.04	0.002	0.00
8	6	7	0.05	0.07	-0.05	-0.07	0.000	0.00
9	6	8	1.32	1.23	-1.31	-1.13	0.013	0.10
10	9	10	0.82	0.85	-0.81	-0.80	0.008	0.05
11	11	12	0.37	0.34	-0.37	-0.33	0.001	0.01
12	11	13	2.82	2.70	-2.80	-2.50	0.017	0.20
Total:							0.064	0.61

  

SnonL =  
93.0128

PnonL =  
47.1976

fp\_nonL =  
0.5074

QnonL =  
80.1484

=====  
=====

| System Summary |

=====

=====  
=====

How many?

-----

Buses	13
Generators	2
Committed Gens	2
Loads	7
Fixed	6
Dispatchable	0
Total NON_LOAD	1
Shunts	1
Branches	12
Transformers	7
Areas	1
Number bus NON_LOAD	7

Maximum

-----

=====  
=====

| Bus Data |

=====

bus	V1(L-N)	V3(L-N)	V5(L-N)	V7(L-N)	THDv[%]
1	39841.6	3.90779	8.78616	24.2485	0.0675322
2	7933.87	5.04674	11.3454	31.3085	0.437868
3	276.342	0.175434	0.392831	1.07771	0.432843
4	39799.7	5.08137	11.4173	31.5045	0.0878355
5	7930.59	5.21932	11.7335	32.3815	0.453062
6	7928.78	5.30164	11.8481	32.4101	0.453726
7	236.506	1.43414	2.17	2.27777	1.92289
8	2406.88	1.59755	3.51898	9.42669	0.435292
9	7928.67	5.21793	11.7298	32.369	0.452997
10	272.881	0.178919	0.399251	1.08986	0.443388
11	7925.59	5.21562	11.7233	32.3465	0.452862
12	271.683	0.178652	0.400956	1.1038	0.450856
13	1394.89	0.912443	2.02685	5.49698	0.437662

**- Caso 2: CFL – L2P14W**

MATPOWER Version 5.1, 20-Mar-2015 -- AC Harmonic Power Flow Calculation  
 MATPOWER Version 5.1, 20-Mar-2015 -- AC Power Flow (Newton)  
 Newton's method power flow converged in 3 iterations.  
 Converged in 0.05 seconds

=====  
 | System Summary |  
 =====

How many?	How much?	P (MW)	Q (MVar)
Buses	13 Total Gen Capacity	200.0	0.0 to 100.0
Generators	2 On-line Capacity	200.0	0.0 to 100.0
Committed Gens	2 Generation (actual)	8.3	2.1
Loads	7 Load	8.2	7.4
Fixed	7 Fixed	8.2	7.4
Dispatchable	0 Dispatchable	-0.0 of -0.0	-0.0
Shunts	1 Shunt (inj)	-0.0	5.9
Branches	12 Losses ( $I^2 * Z$ )	0.06	0.62
Transformers	7 Branch Charging (inj)	-	0.0
Inter-ties	0 Total Inter-tie Flow	0.0	0.0
Areas	1		
		Minimum	Maximum
Voltage Magnitude	0.980 p.u. @ bus 12	1.017 p.u. @ bus 7	
Voltage Angle	-4.22 deg @ bus 8	0.00 deg @ bus 1	
P Losses ( $I^2 * R$ )	-	0.02 MW @ line 11-13	
Q Losses ( $I^2 * X$ )	-	0.21 MVar @ line 4-5	

=====  
 | Bus Data |  
 =====

Bus #	Voltage		Generation		Load	
	Mag(pu)	Ang(deg)	P (MW)	Q (MVar)	P (MW)	Q (MVar)
1	1.000	0.000*	6.26	0.57	-	-
2	0.995	-1.998	2.00	1.49	-	-
3	0.996	-3.085	-	-	0.60	0.53
4	0.999	-0.102	-	-	-	-
5	0.995	-2.011	-	-	2.24	2.00
6	0.994	-2.011	-	-	-	-
7	1.017	-2.107	-	-	0.06	0.08
8	1.001	-4.216	-	-	1.31	1.13
9	0.994	-2.010	-	-	-	-
10	0.984	-3.496	-	-	0.81	0.80
11	0.994	-2.009	-	-	-	-
12	0.980	-2.690	-	-	0.37	0.33

13	1.006	-4.072	-	-	2.80	2.50		
			-----	-----	-----	-----		
		Total:	8.26	2.05	8.19	7.37		
=====								
Branch Data								
=====								
Brnch From To From Bus Injection To Bus Injection Loss (I^2 * Z)								
#	Bus	Bus	P (MW)	Q (MVAr)	P (MW)	Q (MVAr)	P (MW)	Q (MVAr)
-----	-----	-----	-----	-----	-----	-----	-----	-----
1	1	4	6.26	0.57	-6.25	-0.55	0.005	0.01
2	2	3	0.60	0.55	-0.60	-0.53	0.004	0.02
3	2	5	1.40	0.93	-1.40	-0.93	0.000	0.00
4	4	5	6.25	0.55	-6.24	-0.34	0.012	0.21
5	5	6	1.39	1.32	-1.39	-1.32	0.000	0.00
6	5	9	0.82	0.85	-0.82	-0.85	0.000	0.00
7	5	11	3.19	3.04	-3.19	-3.04	0.002	0.00
8	6	7	0.06	0.08	-0.06	-0.08	0.000	0.00
9	6	8	1.32	1.23	-1.31	-1.13	0.013	0.10
10	9	10	0.82	0.85	-0.81	-0.80	0.008	0.05
11	11	12	0.37	0.34	-0.37	-0.33	0.001	0.01
12	11	13	2.82	2.70	-2.80	-2.50	0.017	0.20
							-----	-----
						Total:	0.064	0.62
SnonL =								
113.1107								
PnonL =								
60.8030								
fp_nonL =								
0.5376								
QnonL =								
95.3783								
=====								
System Summary								
=====								
How many?								
-----								
Buses			13					
Generators			2					
Committed Gens			2					



## APÉNDICE VI

### Ficheros de salida en PSpice

A continuación se presentan los ficheros que contienen los datos de salida de la simulación en PSpice.

#### - Componentes de Fourier para construir el diagrama de barras:

DC COMPONENT = 7.7401E-04					
HARMONIC NO	FREQUENCY (HZ)	FOURIER COMPONENT	NORMALIZED COMPONENT	PHASE (DEG)	NORMALIZED PHASE (DEG)
1	6.0000E+01	1.4418E+02	1.0000E+00	-1.6034E+02	0.0000E+00
2	1.2000E+02	1.5707E-02	1.0894E-04	-1.3617E+02	1.8452E+02
3	1.8000E+02	1.2927E+02	8.9655E-01	5.9428E+01	5.4046E+02
4	2.4000E+02	2.6107E-02	1.8107E-04	8.0932E+01	7.2231E+02
5	3.0000E+02	1.0365E+02	7.1886E-01	-7.9284E+01	7.2243E+02
6	3.6000E+02	2.8871E-02	2.0024E-04	-5.7266E+01	9.0480E+02
7	4.2000E+02	7.4175E+01	5.1446E-01	1.4506E+02	1.2675E+03
8	4.8000E+02	2.5422E-02	1.7632E-04	1.7041E+02	1.4532E+03
9	5.4000E+02	4.7855E+01	3.3191E-01	1.4798E+01	1.4579E+03
10	6.0000E+02	1.9855E-02	1.3771E-04	4.6136E+01	1.6496E+03
11	6.6000E+02	2.9231E+01	2.0274E-01	-1.0765E+02	1.6561E+03
12	7.2000E+02	1.5343E-02	1.0641E-04	-7.2238E+01	1.8519E+03
13	7.8000E+02	1.8334E+01	1.2716E-01	1.3626E+02	2.2207E+03
14	8.4000E+02	1.1446E-02	7.9386E-05	1.6955E+02	2.4144E+03
15	9.0000E+02	1.1555E+01	8.0139E-02	2.1589E+01	2.4267E+03
TOTAL HARMONIC DISTORTION = 1.3263E+02 PERCENT					

#### - Valores en el dominio del tiempo para construir el gráfico de la forma de onda de la corriente en la carga no lineal (CFL):

TIME	V(1,0)	V(4,0)	I(Vdc)
5.000E-01	3.266E+02	3.305E+02	8.657E+01
5.000E-01	3.266E+02	3.305E+02	8.657E+01
5.000E-01	3.266E+02	3.305E+02	8.604E+01
5.000E-01	3.266E+02	3.305E+02	8.604E+01
5.000E-01	3.266E+02	3.304E+02	8.500E+01
5.000E-01	3.266E+02	3.304E+02	8.500E+01
5.000E-01	3.266E+02	3.304E+02	8.345E+01

5.000E-01	3.266E+02	3.304E+02	8.294E+01
5.000E-01	3.266E+02	3.304E+02	8.294E+01
5.000E-01	3.266E+02	3.304E+02	8.294E+01
5.000E-01	3.266E+02	3.303E+02	8.143E+01
5.000E-01	3.266E+02	3.303E+02	8.093E+01
5.000E-01	3.266E+02	3.303E+02	8.043E+01
5.000E-01	3.266E+02	3.303E+02	7.993E+01
5.000E-01	3.266E+02	3.302E+02	7.942E+01
5.000E-01	3.266E+02	3.302E+02	7.893E+01
5.000E-01	3.266E+02	3.302E+02	7.893E+01
5.000E-01	3.266E+02	3.302E+02	7.893E+01
5.000E-01	3.266E+02	3.302E+02	7.748E+01
5.000E-01	3.266E+02	3.301E+02	7.700E+01
		:	
5.200E-01	1.056E+02	1.056E+02	-1.001E-07
5.200E-01	1.054E+02	1.054E+02	-1.007E-07
5.200E-01	1.051E+02	1.051E+02	-1.013E-07
5.200E-01	1.049E+02	1.049E+02	-1.019E-07
5.200E-01	1.047E+02	1.047E+02	-1.026E-07
5.200E-01	1.046E+02	1.046E+02	-1.028E-07
5.200E-01	1.046E+02	1.046E+02	-1.028E-07
5.200E-01	1.040E+02	1.040E+02	-1.044E-07
5.200E-01	1.037E+02	1.037E+02	-1.050E-07
5.200E-01	1.035E+02	1.035E+02	-1.056E-07
5.200E-01	1.033E+02	1.033E+02	-1.062E-07
5.200E-01	1.030E+02	1.030E+02	-1.069E-07
5.200E-01	1.028E+02	1.028E+02	-1.075E-07
5.200E-01	1.026E+02	1.026E+02	-1.081E-07
5.200E-01	1.023E+02	1.023E+02	-1.087E-07
5.200E-01	1.022E+02	1.022E+02	-1.089E-07
5.200E-01	1.022E+02	1.022E+02	-1.089E-07
5.200E-01	1.016E+02	1.016E+02	-1.144E-07
5.200E-01	1.014E+02	1.014E+02	-1.165E-07
5.200E-01	1.012E+02	1.012E+02	-1.186E-07